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## Silicon Surface Modification Using $C_4F_8 + O_2$ Plasma for Nano-Imprint Lithography

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The investigation of  $C_4F_8+O_2$  feed gas composition on both plasma parameters and plasma treated silicon surface characteristics was carried out. The combination of plasma diagnostics by Langmuir probes and plasma modeling indicated that an increase in  $O_2$  mixing ratio results in monotonically decreasing densities of  $CF_x$  (x=1-3) radicals as well as in non-monotonic behavior of F atom density. The surface characterization by X-ray photoelectron spectroscopy and contact angle measurements showed that the  $C_4F_8+O_2$  mixtures with less than 60%  $O_2$  result in modification of Si surfaces due to the deposition of the FC polymer films while the change of  $O_2$  mixing ratio in the range of 30%–60% provides an effective adjustment of the surface characteristics such as surface energy, contact angle, etc. Copyright: American Scientific Publishers

**Keywords:** C<sub>4</sub>F<sub>8</sub> Plasma, Treatment, Fluorocarbon Polymer, Surface Modification.

## 1. INTRODUCTION

Nano-imprint lithography (NIL) is one of the promising technologies for fast reproducing nano-scale patterns on the large-area wafers. <sup>1,2</sup> In this technology, the mold made from silicon, silicon dioxide or quartz is simply pressed into a resist and then, is released back leaving the required pattern in the mask. Since the resist often adheres to the mold, the NIL process suffers from several critical problems such as pattern deformation, non-uniform printing and production of residual layers.<sup>3</sup> In fact, all these problems are connected with the mold quality. That is why, the optimization of the mold properties is very important for improving the overall NIL technology.

Generally, in order to minimize the adhesion of resist to the mold surface, the mold needs to have low surface energy. Several researches have studied the modification of the mold surfaces by the polymer-forming fluorocarbon plasmas.<sup>4,5</sup> Particularly, it was found that, after the plasma treatment, the mold surface characteristics are strongly determined by the thickness and chemical composition of

In this work, we attempted both experimental and model-based study of the relationships between the initial composition of  $C_4F_8+O_2$  gas mixture, densities of plasma active species and properties of Si surfaces treated with different  $C_4F_8/O_2$  mixing ratios. The choice of  $C_4F_8$  was because it is known as a strongly polymerizing gas under the plasma conditions.<sup>6-8</sup> At the same time, the  $O_2$  is frequently used as the additive gas in fluorocarbon-based plasmas for suppressing the polymerization.<sup>6-8</sup> Therefore, it can be expected that the variation in  $C_4F_8/O_2$  mixing ratio at constant total gas pressure and input power may be an effective tool for adjusting the properties of the deposited FC polymer films.

the deposited fluorocarbon (FC) polymer film. It is obvious that the properties of the FC polymer film (and thus, the properties of the mold itself), may be adjusted by plasma parameters, type and composition of a feed gas. Unfortunately, in published works, the relationship between the plasma parameters and the polymer characteristics were not investigated in detail. Such situation retards the development of NIL technology.

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# 2. EXPERIMENTAL DETAILS AND MODELING

## 2.1. Experimental Setup and Procedures

The experiments were performed in a planar inductively coupled plasma (ICP) reactor with a cylindrical chamber (r=15 cm), made from anodized aluminum. A 5-turn-copper coil was located on the top of the chamber, above the 10-mm-thick horizontal quartz window. The coil was connected to a 13.56 MHz power supply in order to sustain the plasma. The distance between the window and the bottom electrode, which was used as a substrate holder, was l=12.8 cm. Since the bottom electrode was not biased, it appeared under the floating potential. During the experiments, we used a fixed total gas flow rate (q=30 sccm), gas pressure (p=10 mTorr), and input power  $(W_{\text{inp}}=600 \text{ W})$ . The input power density  $W'=W_{\text{inp}}/\pi r^2 l$  then became 0.6 W/cm³. The  $C_4F_8+O_2$  gas compositions were set by adjusting the partial flow rates.

The Si(100) samples with the size of about  $2 \times 2$  cm² were placed in the center of the bottom electrode. The temperature of the bottom electrode was stabilized at 17 °C using a water-flow cooling system. The processing time  $\tau$  was 30 s. Both treated and reference (non-treated) silicon surfaces were examined using the X-ray photoelectron spectroscopy (XPS) and contact angle measurements. The XPS was provided by VG Scientific ESCALAB 200R with Mg  $K_{\alpha}$  1253.6 eV radiation operating at 260 W. The binding energies were calibrated using C(1s) peak at 284.5 eV. The contact angles were measured at room temperature using the drop shape analysis system (DSA-100, KRUSS) with polar (de-ionized water) and non-polar (CH<sub>2</sub>I<sub>2</sub>) liquids. Then, the free surface energy was calculated through the Owens-Wendt equation.

The plasma parameters were determined by a double Langmuir probe (LP), (DLP2000, Plasmart Inc.). The probe tip was installed through a hole in the sidewall of the chamber, 5.7 cm above the bottom electrode and centered in a radial direction. In order to ensure that the LP results were not affected by the formation of the FC polymer film on the tip surface, the probe tip was cleaned in 50% Ar+ 50% O2 plasma before and after each measurement. The preliminary experiments showed that, even for pure C<sub>4</sub>F<sub>8</sub> plasma, the differences between the continuously recorded current-voltage (I-V) curves did not exceed the standard experimental error for a period of at least 2 min after the plasma was turned on. Since this time was more than  $\tau$ , the measured LP data were adequate to the treatment conditions. The raw I-V curves were treated using the Johnson & Malter's double probe theory<sup>10</sup> and the Allen-Boyd-Reynolds (ABR) approximation for the ion saturation current density.<sup>11</sup> These assume  $J_{+} \approx 0.61 en_{+}v$ , where v is the ion Bohm velocity. The effective ion mass needed to determine v was evaluated simply through the mole fractions of the corresponding neutral species. The output LP data were the electron temperature  $(T_a)$ , ion current

density  $(J_+)$ , floating potential  $(U_f)$ , and total positive ion density  $(n_+)$ .

## 2.2. Plasma Modeling

To obtain the densities and fluxes of the active species, we developed a simplified zero-dimensional model operating with the volume-averaged plasma parameters. Similar to our papers, 12, 13 the model was based on the Maxwellian electron energy distribution function (EEDF), and used the experimental results of  $T_e$  and  $n_{\perp}$  directly as input parameters. Earlier, it was found that, for the given range of process conditions, the electronegativity of both C<sub>4</sub>F<sub>8</sub> and  $O_2$  plasmas is low enough to assume  $n_- \ll n_e \approx n_{\perp}$ . Particularly, Vasenkov et al. 14 reported about  $n_e \approx n_{\text{CF}_2^+} + n_{\text{CF}_2^+}$ in pure  $C_4F_8$  and  $n_e \approx n_{O_2^+}$  in pure  $O_2$  at  $p=2\bar{0}$  mTorr and  $W' = 0.5 \text{ W/cm}^3$ . Also, Rauf and Ventzek<sup>15</sup> measured  $n_{-}/n_{e} \sim 0.06$  for 98% C<sub>4</sub>F<sub>8</sub> + 2% Ar and  $n_{-}/n_{e} \sim 0.03$ for 50%  $C_4F_8 + 50\%$  Ar ICP at p = 10 mTorr and W' =0.6 W/cm<sup>3</sup>. And finally, Efremov et al. noted  $n_{-}/n_{e} \sim$ 0.2 for pure O<sub>2</sub> ICP at p = 10 mTorr and W' = 0.1 W/cm<sup>3</sup>. Since the last W' is much less than that in current study, we can assume  $n_{-}/n_{e} < 0.1$  with confidence. That is why, our model accounted only for the chemistry of neutral species (Table I).17-19

The steady-state (dn/dt = 0) densities of neutral species were obtained from the system of chemical kinetics equations in the general form of  $R_F - R_D = (k_s + 1/\tau_R)n$ , where  $R_F$  and  $R_D$  are the volume-averaged formation and decay rates in bulk plasma for a given type of species, n is their density,  $k_S$  is the first-order heterogeneous decay rate coefficient, and  $\tau_R = \pi r^2 lp/q$  is the residence time. The rate coefficients for electron impact reactions (R1-R23), were calculated as functions of T<sub>e</sub> using fitting expressions in the form of  $k = AT_e^B \exp(-C/T_e)^{17-19}$ The rate coefficients for R24-R63 were taken from the NIST chemical kinetics database.<sup>20</sup> The rate coefficients for the heterogeneous loss of atoms and radicals R64-R70 were calculated as  $k_S = [(\Lambda^2/D) + (2r/\gamma v_T)]^{-1}$ , where D is the effective diffusion coefficient,  $^{30}$   $\Lambda^{-2}$  =  $(2.405/r)^2 + (\pi/l)^2$  is the diffusion length,<sup>21</sup> and  $v_T =$  $(8k_BT/\pi m)^{1/2}$ . The sticking probabilities  $\gamma$  were obtained from Refs. [16, 17]. The temperature of the neutral ground-state species T was assumed to be independent of the feed gas composition. 16-18 Since experimental data on T were not extracted during this study, we took T =700 K as the typical value for close ranges of p and W' in ICP etching reactors with similar geometry. 16,17 All reaction pathways between the adsorbed (marked by the "s" index) and gaseous species inside R64-R69 were assumed to have equal probabilities of occurrence. The rate coefficients for the heterogeneous loss of ions R71-R73 were calculated as  $k_S = v/d_c$ , where  $d_c = 0.5rl/(rh_l + lh_r)$ . The correction factors for axial  $(h_1)$  and radial  $(h_r)$ sheath sizes are given by the low pressure diffusion theory.21

**Table I.** Reduced reaction set for the modeling of neutral species chemistry in  $C_4F_8+O_2$  plasmas.

		Rate coefficient [cm <sup>3</sup> /s]					
Process		$\varepsilon_{\mathrm{th}} \; [\mathrm{eV}]$	A	В	С		
Electro	n-impact reactions						
R1	$C_4F_8 + e = 2C_2F_4 + e$	2.16	$8.71 \times 10^{-8}$	0.042	8.572		
R2	$C_4F_8 + e = C_3F_6 + CF_2 + e$	3.25	$8.71 \times 10^{-8}$	0.042	8.572		
R3	$C_3F_6 + e = C_2F_4 + CF_2 + e$	4.53	$1.07 \times 10^{-8}$	0.23	7.451		
R4	$C_2F_4 + e = 2CF_2 + e$	3.06	$1.32 \times 10^{-8}$	0.412	6.329		
R5	$C_2F_4 + e = C_2F_3^+ + F + 2e$	15.57	$3.03 \times 10^{-9}$ $3.30 \times 10^{-8}$	0.874 0.412	16.41 6.329		
R6 R7	$C_2F_3 + e = CF_2 + CF + e$ $CF_4 + e = CF_3 + F + e$	3.06 5.60	$1.38 \times 10^{-8}$	0.412	16		
R8	$CF_4 + e = CF_3 + F + e$ $CF_4 + e = CF_2 + 2F + e$	9.50	$2.22 \times 10^{-10}$	0.99	14.77		
R9	$CF_4 + e = CF_3^+ + F + 2e$	15.9	$9.36 \times 10^{-8}$	0	20.4		
R10	$CF_4 + e = CF_3 + F^+ + 2e$	23.10	$9.79 \times 10^{-10}$	0.94	34.67		
R11	$CF_3 + e = CF_2 + F + e$	3.80	$6.48 \times 10^{-8}$	-0.959	11.25		
R12	$CF_2 + e = CF + F + e$	5.40	$8.11 \times 10^{-9}$	0.386	8.739		
R13	$CF_2 + e = C + 2F + e$	11.00	$1.39 \times 10^{-8}$	-1.164	49.87		
R14	CF + e = C + F + e	5.60	$1.63\times10^{-8}$	-0.002	13.05		
R15	$F_2 + e = 2F + e$	4.34	$1.08\times10^{-8}$	-0.296	4.464		
R16	$O_2 + e = 2O + e$	6.40	$1.52 \times 10^{-9}$	0	4.15		
R17	$O_2 + e = O + O(1d) + e$	8.57	$2.04 \times 10^{-8}$	0	8.18		
R18	$CO_2 + e = CO + O + e$	13.50	$1.87 \times 10^{-8}$	0	13.89		
R19	CO + e = C + O + e	13.50	$1.87 \times 10^{-8}$	0	13.89		
R20	O + e = O(1d) + e	1.97	$4.47 \times 10^{-9}$	0	2.29		
R21	FO + e = F + O + e	4.30	$6.16 \times 10^{-9}$	0	4.30		
R22	CFO + e = CO + F + e	5.40 3.80	$8.11 \times 10^{-9}$ $6.48 \times 10^{-8}$	0.386	8.739		
R23	$CF_2O + e = CFO + F + e$			-0.959	11.25		
	om-molecular, radical-molecu			eactions			
R24	$C_2F_3 + F = C_2F_4$ $C_2F_4 + O = CF_2O + CF_2O$	$1.00 \times 10$		oina Ta	chno		
R25 R26	$C_2F_4 + O = CF_2O + CF_2$ $C_2F_4 + O(1d) = CF_2O + CF_2$		) <del>1</del> 45.145.				
R27	$C_2F_4 + G(Id) = GF_2G + GF_2$ $C_2F_4 + F = CF_2 + CF_3$		) <sup>-11</sup> Copyri				
R28	$C_2F_4 + C = C_2F_3 + CF$	$1.00 \times 10^{-1}$		9111. 7 11			
R29	$F_2 + CF_3 = CF_4 + F$	$6.31 \times 10^{-1}$					
R30	$F_2 + CF_2 = CF_3 + F$	$7.94 \times 10^{-2}$					
R31	$F_2 + CF = CF_2 + F$	$3.98 \times 10^{-2}$					
R32	$F_2 + O = FO + F$	$1.00 \times 10$	$)^{-16}$				
R33	$F_2 + O(1d) = FO + F$	$7.94 \times 10^{-2}$					
R34	$F_2 + CFO = CF_2O + F$	$5.01 \times 10^{-1}$					
R35	$CF_3 + F = CF_4$	$1.00 \times 10$					
R36	$CF_3 + O = CF_2O + F$	$3.16 \times 10^{-1}$					
R37	$CF_3 + O(1d) = CF_2O + F$	$3.16 \times 10^{-1}$					
R38	$CF_2 + F = CF_3$	4.17 × 10					
R39	$2CF_2 = C_2F_4$	5.01 × 10					
R40	$CF_2 + CF = C_2F_3$	$1.00 \times 10$					
R41	$CF_2 + O = CFO + F$	$3.16 \times 10$					
R42 R43	$CF_2 + O(1d) = CFO + F$ $CF_2 + O = CO + 2F$	$3.16 \times 10$ $3.98 \times 10$					
R44	$CF_2 + O = CO + 2F$ $CF_2 + O(1d) = CO + 2F$	$3.98 \times 10$					
R45	$CF + F = CF_2$	$5.00 \times 10^{-3.00} \times 10^{-3.00$					
R46	CF + O = CO + F	$6.31 \times 10^{-10}$					
R47	CF + O(1d) = CO + F	$2.00 \times 10^{-10}$					
R48	$CF + O_2 = CFO + O$	$3.16 \times 10^{-2}$					
R49	$FO + O = F + O_2$	$2.51 \times 10^{-2}$					
R50	$FO + O(1d) = F + O_2$	$5.01 \times 10^{-1}$					
R51	$FO + FO = 2F + O_2$	$2.51 \times 10^{-2}$	$)^{-12}$				
R52	$2FO = F_2 + O_2$	$2.51 \times 10^{-2}$					
R53	$CFO + CF_3 = CF_4 + CO$	$1.00 \times 10^{-1}$					
R54	$CFO + CF_3 = CF_2O + CF_2$	$1.00 \times 10^{-1}$					
R55	$CFO + CF_2 = CF_3 + CO$	$3.16 \times 10^{-2}$					
R56	$CFO + CF_2 = CF_2O + CF$	$3.16 \times 10^{-10}$					
R57	$CFO + O = CO_2 + F$	1.00 × 10					
R58	$CFO + O(1d) = CO_2 + F$	$1.00 \times 10$					
R59	$2CFO = CF_2O + CO$	$1.00 \times 10^{-1}$	, ··				

Table 1. Continued.

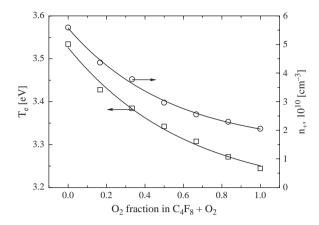
		Rate coefficient [cm³/s]				
Process		$\varepsilon_{\text{th}} [\text{eV}]$	A	В	С	
R60	$CFO + F = CF_2O$	$7.94 \times 10^{-11}$				
R61	$CF_2O + O(1d) = F_2 + CO_2$	$2.00 \times 10^{-11}$				
R62	$C + O_2 = CO + O$	$1.58 \times 10^{-11}$				
R63	CO + F = CFO	$1.29 \times 10^{-11}$				
Heter	ogeneous reactions					
R64	$F = F(s) + CF_3 = CF_4$ $+ CF_2 = CF_3$ $+ CF = CF_2$ $+ F = F_2$ $+ C = CF$ $+ C_2F_3 = C_2F_4$ $+ O = FO$	$f(\gamma), \ \gamma = 0.0$	05			
R65	$CF_3 = CF_3(s) + F = CF_4$ $+ CF = C_2F_4$ $+ C = C_2F_3$	$f(\gamma), \ \gamma = 0.0$	05			
R66	$CF_2 = CF_2(s) + F = CF_3$ $+ CF_2 = C_2F_4$ $+ CF = C_2F_3$ $+ O = CF_2O$	$f(\gamma), \ \gamma = 0.$	1			
R67	$CF = CF(s) + F = CF_2$ + $CF_2 = C_2F_3$ + $CF_3 = C_2F_4$ + $O = CFO$	$f(\gamma), \gamma = 0.$	1			
R68	$C = C(s) + F = CF$ $+ CF_3 = C_2F_3$ $+ O = CO$	$f(\gamma), \ \gamma = 1$				
	$SQ = O(s) + Q = Q_{20}$ Unive 5 Jan 20+F = FO 3:30 tific Pub + C = CO + CF = CFO	$f(\gamma), \gamma = 0.$	1			
D.70	$+CF_2 = CF_2O$					
	$O(1d) = O$ $f(\gamma), \gamma = 1$	(T)	0.5.1	// 1 . 1	1	
	$CF_3^+ = CF_3$ $v/d_c$ , where $v \approx$	$\sqrt{eI_e/m_i} d_c =$	0.5 <i>rl</i>	$r(rh_l+l)$	$n_r$ )	
	$F^+ = F$					
R73	$C_2F_3^+ = C_2F_3$					

The model quality was preliminarily tested using the experimental data on both  $CF_2$  and CF radical densities in  $C_4F_8/Ar$  plasma from Ref. [15]. This work was selected because it also provides the measurements of  $T_e$  and  $n_e$ , which are required as input model parameters. As a result, the reasonable agreement between measured and model-predicted densities was obtained.

## 3. RESULTS AND DISCUSSION

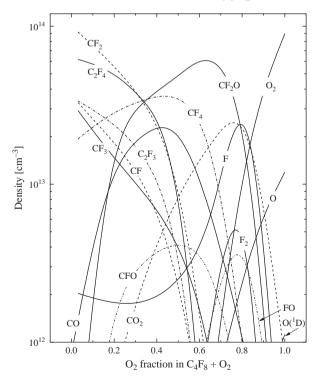
## 3.1. Plasma Characterization

Figure 1 represents the results of plasma diagnostics using Langmuir probes. From Figure 2, it can be seen that an increase in  $O_2$  fraction in a feed gas results in decreasing  $T_e$  in the ranges of 3.5–3.2 eV. The reason for this is an increase in the electron energy loss due to the low-threshold excitations (vibrational, electronic) for  $O_2$  and other molecular species, which appear in a gas phase as products of plasma chemical reactions. The measured total density of positive ions (and thus, the electron density,



**Figure 1.** Measured electron temperature  $(T_e)$  and total positive ion density  $(n_+)$  as functions of  $O_2$  fraction in  $C_4F_8+O_2$  gas mixture. The remaining process conditions are p=10 mTorr,  $W_{\rm inp}=600$  W and q=30 sccm.

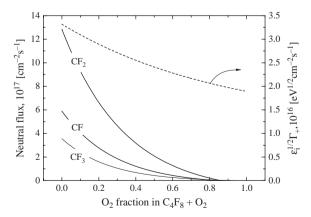
since  $n_+\approx n_e$ ) also decreases toward O<sub>2</sub>-rich plasmas  $(n_+=5.6\times 10^{10}-2.1\times 10^{10}~{\rm cm}^{-3}~{\rm for}~0-100\%~{\rm O}_2).$  In our opinion, such effects are caused by a combination of at least two phenomena. First, the decreasing  $T_e$  suppresses ionization through decreasing the ionization rate coefficients  $k_{iz}$  for all types of neutral species. The high sensitivity of  $k_{iz}$  to  $T_e$  is because  $\varepsilon_{iz}\approx 12-15~{\rm eV}>\langle\varepsilon\rangle$ , where  $\varepsilon_{iz}$  is the threshold energy for ionization,  $^{17,19}$  and  $\varepsilon$  and  $\varepsilon$  are  $(3/2)T_e$  is the mean electron energy for Maxwellian EEDF. And secondly, the substitution of Ar for O<sub>2</sub> probably



**Figure 2.** Model-predicted densities of neutral species as functions of  $O_2$  fraction in  $C_4F_8+O_2$  gas mixture. The process conditions correspond to Figure 1.

results in an increase in the densities of electronegative species, caused by both the  $O_2$  itself and oxygencontaining reaction products. This accelerates the decay of the positive ions and electrons through ion–ion recombination and dissociative attachment, respectively. It is important to note also that the behaviors of both  $T_e$  and  $n_+$  versus  $O_2$  mixing ratio shown in Figure 1 are in good qualitative agreement with previously published data.  $^{14,22}$ 

Figure 2 illustrates the influence of O<sub>2</sub> content in the  $C_4F_8 + O_2$  gas mixture on the densities of neutral species. In pure C<sub>4</sub>F<sub>8</sub> plasma, the dominant neutral species are  $C_2F_4$ ,  $C_2F_3$  and  $CF_x$  (x = 1-3) radicals. The high densities of C<sub>2</sub>F<sub>4</sub>, C<sub>2</sub>F<sub>3</sub> and CF<sub>2</sub> are related with the direct formation of these species in R1-R6 with the participation of the original C<sub>4</sub>F<sub>8</sub> molecules and their first-step dissociation products. The domination of CF<sub>2</sub> over other types of neutral species results from the significant contribution to their total formation rate from the sides of R27, R31, and R45. The high formation rate and density of CF<sub>3</sub> radicals is provided not only by the primary electron-impact reactions R7 and R10, but also by R27, R38, and R66 because of the high densities of C<sub>2</sub>F<sub>4</sub> and CF<sub>2</sub>, respectively. And finally, the density of CF radicals is lifted up due to their high formation rates in electron-impact reactions R6 and R12 with the participation of C<sub>2</sub>F<sub>3</sub> and CF<sub>2</sub>. The combination of high values of  $n_{CF_3}$ ,  $n_{CF_2}$  and  $n_{CF}$  makes the  $C_4F_8$  plasma a strongly polymerizing system. This fact has been repeatedly confirmed by experiment.  $^{18,23,24}$  The addition of  ${\rm O_2}$ Sto C<sub>4</sub>F<sub>8</sub> introduces additional dissociation mechanisms for C<sub>2</sub>F<sub>4</sub> (R25, R26), CF<sub>3</sub> (R36, R37), CF<sub>2</sub> (R41–R44) and CF (R46–R48) increasing the total loss rates for these species compared with non-oxygenated plasmas. As a result, their densities (Fig. 2) and fluxes (Fig. 3) decrease faster that linearly (for example, by 8 times for  $CF_2$  at 0–50%  $O_2$ ) with increasing O<sub>2</sub> fraction in a feed gas. Simultaneously, since the reactions R36, R37, R41-R44 and R46-R48 follow the scheme of  $CF_x + O \rightarrow CF_{x-1}O + F$ , the addition of O<sub>2</sub> accelerated the formation of F atoms and results in



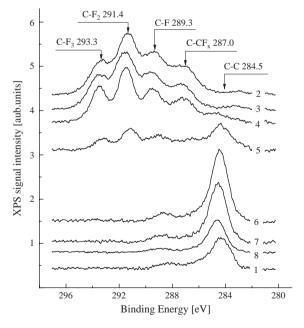
**Figure 3.** Model-predicted fluxes of polymer-forming species ( $CF_x$  radicals) and ion energy flux as functions of  $O_2$  fraction in  $C_4F_8 + O_2$  gas mixture. The process conditions correspond to Figure 1.

the non-monotonic behavior of  $n_F$ . The ion energy flux characterized by the parameter  $\sqrt{\varepsilon_i}\Gamma_+$ ,  $^{12,25,26}$  where  $\varepsilon_i\approx eU_f$ —ion energy and  $\Gamma_+\approx J_+/e$ —ion flux, also decreases toward  $O_2$ -rich plasmas. In our case, the low energy ions ( $\varepsilon_i=23$ –19 eV for 0–100%  $O_2$ ) cannot provide the sputtering of both FC film or Si surfaces. However, these can "open" the C–F bonds in the previously adsorbed fluorocarbon species ( $\varepsilon_{C-F}=552$  kJ/mol or 5.8 eV<sup>27</sup>) and thus, can increase the polymerization probability. Therefore, an increase in  $O_2$  mixing ratio in the  $C_4F_8+O_2$  gas mixture definitely suppresses the deposition of the FC polymer film and shifts the general heterogeneous reaction pathway from polymerization to etching.

It is worth mentioning that the behaviors of the CF, CF<sub>2</sub>, and CF<sub>2</sub>O species shown in Figure 2 are in good agreement with the measured values reported by Li et al.<sup>28</sup> Also, the model-predicted fluxes of CF<sub>x</sub> radicals from Figure 3 shows the same behavior with the FC film deposition rate<sup>28</sup> while the non-monotonic F atom flux corresponds to the non-monotonic Si etching rate.<sup>28</sup> All these allow us to conclude that our model provides an adequate description of the main kinetic effects determining the composition of  $C_4F_8+O_2$  plasma.

#### 3.2. Surface Characterization

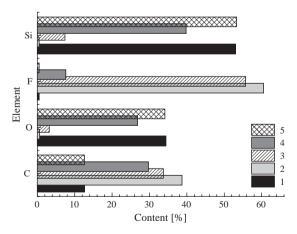
Figure 4 shows the C(1s) XPS narrow scan spectra for Si surfaces treated with different gas mixing ratios. It can be seen that the surface treated in 100% of C<sub>4</sub>F<sub>8</sub> plasma shows the group of peaks in the range of 285–295 eV



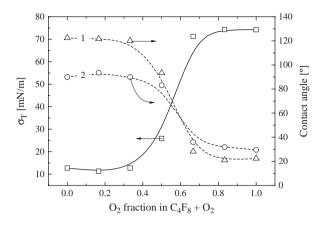
**Figure 4.** Measured C(1s) XPS narrow scan spectra for Si surfaces treated with different gas mixing ratios: 1-Reference (non-treated) sample, 2-100% C<sub>4</sub>F<sub>8</sub>, 3-83% C<sub>4</sub>F<sub>8</sub>+17% O<sub>2</sub>, 4-67% C<sub>4</sub>F<sub>8</sub>+33% O<sub>2</sub>, 5-50% C<sub>4</sub>F<sub>8</sub>+50% O<sub>2</sub>, 6-33% C<sub>4</sub>F<sub>8</sub>+67% O<sub>2</sub>, 7-17% C<sub>4</sub>F<sub>8</sub>+83% O<sub>2</sub>, 8-100% O<sub>2</sub>. The process conditions correspond to Figure 1.

which belong to various fluorocarbon species. The presence of  $C-CF_x$  bonds at 287.0 eV directly points out on the polymer-like structure of the deposited film. An increase in  $O_2$  fraction in a feed gas results in decreasing intensities for all fluorocarbon peaks while after 50%  $O_2$  the C-C peak at 284.5 eV appear in the spectra. Since this peak was also detected on the reference (non-treated) surface as well as did not disappear (in fact, keep the same intensity) after the treatment in pure  $O_2$  plasma, the observed carbon seems to be chemically bonded with Si atoms. This allows one to assume that, for the given treatment time, the  $C_4F_8+O_2$  mixtures with less than 50%  $O_2$  provide the formation of the continuous FC polymer film on the Si surface.

Figure 5 illustrates the overall chemical states for Si surfaces calculated under an assumption that intensity of the XPS peak is proportional to the content of corresponding element. For this purpose, the C(1s), F(1s), O(1s) and Si(2p) peaks were used. It can be seen that the amount of C(1s) decreases monotonically toward  $O_2$ -rich plasmas that corresponds to the transition from C-F bonds in the FC polymer film to C-C bonds in the original surface. The fraction of F(1s) does not reflect the non-monotonic behavior of F atom density, but shows a good correlations with the total CF<sub>r</sub> flux from Figure 3 as well as with the change of C(1s). The amount of bonded oxygen is one and the same for both reference (non-treated) samples and the samples treated in 100% O2 plasma. Also, since the fraction of O(1s) decreases monotonically toward C<sub>4</sub>F<sub>8</sub>-rich plasmas following the behavior of Si(2p), one can conclude that the observed oxygen is not incorporated in the polymer film structure and belongs to the native silicon oxide. The disappearance of both O(1s) and Si(2p) peaks after the treatments with more than 70% C<sub>4</sub>F<sub>8</sub> gas mixtures can be attributed to the formation of thick continuous FC polymer film. All these allow one to assume that the variations in O<sub>2</sub> content in a feed gas do not change the



**Figure 5.** Chemical compositions for Si surfaces treated with different gas mixing ratios: 1-Reference (non-treated) sample, 2-100%  $C_4F_8$ , 3-67%  $C_4F_8+33\%$   $O_2$ , 4-33%  $C_4F_8+67\%$   $O_2$ , 5-100%  $O_2$ . The process conditions correspond to Figure 1.



**Figure 6.** Measured contact angles (1-de-ionized water, 2-diiodomethane) and calculated free surface energy as functions of  $O_2$  fraction in  $C_4F_8+O_2$  gas mixture. The process conditions correspond to Figure 1.

chemical structure of the FC polymer film, but influence the film thickness only.

From Refs. [9, 29], it is known that many surface characteristics (chemical activity, wettability, adhesion ability) are closely linked with the free surface energy  $\sigma_T$ . Speaking simply, the higher  $\sigma_T$  values correspond to "active" surface while the lower  $\sigma_T$  allows one to speak about an "inert" surface. From Figure 6, it can be seen that the transition from pure C<sub>4</sub>F<sub>8</sub> to pure O<sub>2</sub> feed gas results in increasing  $\sigma_T$  in the range of 12.7–74.2 mN/m. This indicates that the plasma treated surface changes from the hydrophobic state to the hydrophilic one and/or becomes to be more adhesive for photoresists. The constancy of  $\sigma_T$ for less than 30% O<sub>2</sub> gas mixtures may be attributed to the formation of thick continuous FC polymer film with constant chemical composition. A rapid growth in  $\sigma_T$  for 30-60% O<sub>2</sub> is probably due to the transition to the noncontinuous (island-like) film structure where an effective island size decreases with increasing  $O_2$  fraction in a feed gas. Also, the same result may be obtained for thin continuous films if the film properties are affected by the substrate. And finally, the constancy of  $\sigma_T$  for more than 60% O<sub>2</sub> gas mixtures in our opinion corresponds to original Si surface with a negligible coverage by the FC polymer. Therefore, the  $C_4F_8 + O_2$  mixtures with less than 60%  $O_2$ result in modification of Si surfaces due to the deposition of the FC polymer films while the change of O<sub>2</sub> mixing ratio in the range of 30-60% provides an effective adjustment of the surface characteristics.

## 4. CONCLUSIONS

In this work, we carried out the Si surface modification by inductively coupled plasma  $C_4F_8/O_2$  plasma treatment for the demolding process in nano-imprint lithography. We also investigated the influence of  $O_2$  fraction in  $C_4F_8+O_2$  feed gas on both plasma parameters and plasma treated silicon surface characteristics. From plasma diagnostics by

Langmuir probes and plasma modeling, it was found that the transition from  $C_4F_8$ -rich to  $O_2$ -rich plasmas results in monotonically decreasing densities and fluxes of polymerforming species ( $CF_x$  radicals), but in non-monotonic behavior of F atom density. The XPS analysis showed that: (1) the  $C_4F_8+O_2$  mixtures with less than 60%  $O_2$  result in deposition of the FC polymer films; and

(2) the variations in  $O_2$  mixing ratio influence the film thickness only. The measurements of free surface energy allow one to conclude that the change of  $O_2$  mixing ratio in the range of 30–60% provides an effective adjustment of the surface characteristics. For less than 30%  $O_2$  as well as for more than 60%  $O_2$  the plasma treated surfaces keep the constant properties corresponding to thick continuous FC film (low  $\sigma_T$ ) or original surface (high  $\sigma_T$ ), respectively.

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